# Whole Powdern Pattern Modelling (analysis of nanocrystalline materials)

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# WPPM : basics



In traditional methods of analysis we loose the direct contact with the experimental data



This has been the main driving force towards the introduction of Whole Powder Pattern Modelling, aimed at directly extract the information from the experimental pattern

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## Whole Powder Pattern Modelling: WPPM

*WPPM* is based on a direct modelling of the experimental pattern, based on physical models of the microstructure and lattice defects:





#### Pattern built as sum of broadened peaks plus a background





Each peak is synthesised in reciprocal space from its Fourier transform and then remapped into  $2\theta$  space through the use of a suitable interpolation algorithm





 $T^{IP}$ 

pV

 $\{hkl\}$ 

Instrumental Profile

### WPPM: basics

$$I_{\{hkl\}}\left(d^{*}, d_{\{hkl\}}^{*}\right) = k\left(d^{*}\right) \cdot \sum_{hkl} w_{hkl} \int_{-\infty}^{\infty} \mathbb{C}_{hkl}(L) \exp\left(2\pi i L \cdot s_{hkl}\right) dL$$
  
Diffraction profiles result  
from a convolution of effects.  
$$\cdot A_{\{hkl\}}^{S} \cdot A_{\{hkl\}}^{D} \cdot (A_{hkl}^{F} + iB_{hkl}^{F}) \cdot A_{\{hkl\}}^{APB} \cdot (A_{hkl}^{GSR} + iB_{hkl}^{GSR}) \cdot (A_{hkl}^{CF} + iB_{hkl}^{CF}) \cdot$$

Domain size Dislocations

Faulting

Instrumental Profile, Domain Size, Dislocations, Anti-Phase Domain terms are real functions of L (Fourier length), whereas Faulting, Grain Surface Relaxation and fluctuations in the composition give complex (A+iB) contributions

APB

Additional line broadening sources can be included by adding (multiplying) corresponding FTs

Grain surface relaxation

54° Denver X-ray conference Colorado Springs - 2005 - Matteo Leoni  $B_{_{hkl}}^{CF}$ 

Stoichiometry fluctuations

## WPPM: instrumental profile

The following curves, e.g. can be obtained by plotting the half width at half maximum and the gaussian content of the pseudo-Voigt profile for the fit of the  $LaB_6$  SRM 660A standard peaks measured on a Rigaku diffractometer:



# WPPM: instrumental profile

When a pseudo-Voigt curve is used for the modelling, the following expression can be used for the corresponding Fourier cosine coefficients:

$$T_{pV}^{IP}(L) = (1-k) \cdot \exp\left(-\pi^2 \cdot \sigma_s^2 L^2 / \ln 2\right) + k \exp\left(-2\pi \cdot \sigma_s L\right)$$

Sine coefficients are zero if the curve is considered as symmetric. Width ( $\sigma_s$ ) and shape (related to k) parameters for the given reflection (e.g. given Bragg angle) are determined from the parametric description of the instrumental profile.



In a nanocrystalline material, the most important broadening source is perhaps the small size of coherently diffracting domains







Expressions for  $A_c(L,D)$  can be calculated for different crystal shapes by means of the 'ghost' concept of Wilson:



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**Fourier Coefficients:**  $A_i(L) = [M_{i,3}]^{-1} \int_{LK}^{\infty} A_c(L,D) D^3 g_i(D) dD$ 

$$A_{l}(L) = \sum_{n=0}^{3} Erfc \left[ \frac{\ln(L \cdot K^{c}) - \mu - (3 - n)\sigma^{2}}{\sigma\sqrt{2}} \right] \frac{M_{l,3-n}}{2M_{l,3}} \cdot H_{n}^{c} L^{n}$$

$$A_{p}(L) = \sum_{n=0}^{3} \left(\frac{\sigma}{\mu}\right)^{n} \frac{\Gamma\left(\sigma + (3-n), \frac{K^{c}L\sigma}{\mu}\right)}{\Gamma(\sigma+3)} \cdot H_{n}^{c}L^{n}$$

YORK

LOGNORMAL

$$A_{Y}(L) = \sum_{n=0}^{3} \left(\frac{\sigma}{\mu}\right)^{n} \frac{\Gamma\left(\sigma + (4-n), \frac{K^{c}L\sigma}{\mu}\right)}{\Gamma(\sigma+4)} \cdot H_{n}^{c}L^{n}$$



Dislocations are quite often the main kind of lattice defect present in a nanocrystalline material



# WPPM: dislocation contrast

Line broadening due to dislocation is markedly anisotropic (it introduces specific *hkl* dependence)



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### WPPM: dislocation contrast



# WPPM: dislocation contrast

The Fourier coefficients relative to dislocations (average density  $\rho$ , effective outer cut-off radius  $R_e$ , Burgers vector b and average contrasts factor  $\overline{C}_{hkl}$ ) read:

$$A_{\{hkl\}}^{D}(L) = \exp\left[-\frac{1}{2}\pi |b|^{2} \overline{C}_{hkl} \rho d_{\{hkl\}}^{*^{2}} \cdot L^{2} f^{*}(L/R_{e})\right]$$

where  $f^*(L/R_e)$  is Wilkens' function.



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### WPPM: antiphase boundaries





For the presence of anti-phase domain boundaries (where the probability of finding a fault along the chosen direction is  $\gamma$ ):

$$A_{\{hkl\}}^{APB}(L) = \exp\left[-\frac{-2\gamma(|h|+|k|)\cdot L}{d_{hkl}(h^{2}+k^{2}+l^{2})}\right]$$

Only superstructure peak profiles are affected



Line broadening due to faulting is markedly anisotropic (it introduces specific *hkl* dependence)





hkl dependence is different than that seen for dislocations

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For twin and deformation faults in fcc (probability  $\beta$  and  $\alpha$ , respectively):

$$A_{hkl}^{F}(L) = \left(1 - 3\alpha - 2\beta + 3\alpha^{2}\right)^{\left|\frac{1}{2}Ld_{\{hkl\}}^{*}\cdot\frac{L_{o}}{h_{o}^{2}}\sigma_{L_{o}}\right|}$$

$$B_{hkl}^{F}(L) = -\sigma_{L_{o}} \cdot \frac{L}{|L|} \cdot \frac{L_{o}}{|L_{o}|} \cdot \beta / (3 - 6\beta - 12\alpha - \beta^{2} + 12\alpha^{2})^{1/2}$$

The modelling is highly simplified (rough description of the phenomena), but it can be seen that the profile is not symmetrical (a sine term is present).

Each member of the {hkl} family can possibly be broadened, asymmetric and shifted from its Bragg position:



# WPPM simulation: effect of faulting

(111) faulting in *fcc* metal structures  $\alpha$ =2%,  $\beta$ =5%, <D>=59 nm,  $\rho$ =10<sup>13</sup> m<sup>-2</sup>





## WPPM: fingerprint of the effects

$$I_{\{hkl\}}\left(d^*, d_{\{hkl\}}^*\right) = k\left(d^*\right) \cdot \sum_{hkl} w_{hkl} \int_{-\infty}^{\infty} \mathbb{C}_{hkl}(L) \exp\left(2\pi i L \cdot s_{hkl}\right) dL$$
$$\frac{T_{PV}^{IP} A_{\{hkl\}}^S A_{\{hkl\}}^{APB} \left(A_{hkl}^F + i B_{hkl}^F\right) A_{\{hkl\}}^D}{\left(A_{hkl}^F + i B_{hkl}^F\right) A_{\{hkl\}}^D}$$



# WPPM : software

### PM2K is a general problem-independent fit program.

- based on a multiple client/server architecture
- server implements a problem-independent multi-purpose fit routine, driven through a TCP-IP interface
- > plugins are used to extend the functionality of the routine:
  - the WPPM algorithm is built as plug-in for the server
  - broadening models used in WPPM are designed as plugins
  - input/output file type managers are plugins
  - a plugin development kit allows an easy implementation of new models
  - the program uses a versatile input file format

# Possible broadening plugins for WPPM (most of them already implemented):

- > Instrumental broadening
  - Caglioti pV
  - FPA

#### > Size broadening

- HISTOGRAM MODEL
  - (sphere, cube, tetrahedron, octahedron, ellipsoid, hexagonal prism, cylinder, harmonics)
- ANALYTICAL MODEL
  - delta, lognormal, gamma, generalised gamma, York distributions (sphere, cube, tetrahedron, octahedron, ellipsoid, hexagonal prism, cylinder, harmonics)
- Column Length Distribution (a la Bertaut)



#### > Strain broadening

- dislocations (all symmetries) (simplified Wilkens, full Wilkens models)
- dislocations (all symmetries) (harmonics invariant, Green function model)
- dislocation configurations (arrays, pile-ups, walls)
- van Berkum model
- Houska-like (Houska, Adler-Houska, modified Houska)

#### > Effective models (size/strain mix)

• Stephens/Popa

#### > Faulting

- recursion equations (Warren) for fcc, bcc and hcp
- correlation probability
- correlation matrices
- recursive approach (convergence towards DIFFaX<sup>+</sup>)



#### Antiphase Boundaries

- Wilson-Zsoldos finite differences
- Wilson-Zsoldos differential equations

#### > Grain Surface Relaxation

- original model (size-independent relaxation-zone width)
- modified model (size-dependent relaxation)

#### > Additional broadening models

- full micromechanical model
- grain-dependent lattice parameter
- stoichiometry fluctuation

A **plugin development kit** is available (example written in C++) for those willing to implement their models into PM2K. Just throw the plugin in plugins directory and the new function will be automatically available to PM2K.



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# Ball milled nickel powder

- Antiphase domains in Cu<sub>3</sub>Au
- Nanocrystalline cerium oxide
- Ball milled Fe-1.5Mo
- Ball milled fluorite



### ball milled Ni, WPPM





## ball milled Ni, WPPM





# ball milled Ni, WPPM





### ball milled Ni, WPPM results









### ball milled Ni, stored energy




#### ball milled Ni, WPPM domain size distribution





#### ball milled Ni, comparison WPPM-TEM

#### Nickel powder ball milled for 96 h





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#### WPPM application: APBs in Cu<sub>3</sub>Au

# Anti Phase Domains form during the ordering process in $Cu_3Au$ . The o/d process can be thermally activated





#### Antiphase boundaries





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# Disordered phase





# Ordered phase





#### Various models used in WPPM



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## WPPM results

	As received (disordered phase)	Thermally treated (ordered phase)				
Average dislocation density, $\rho$ [m <sup>-2</sup> ]	9.2(6) x10 <sup>15</sup>	4.7(10) x10 <sup>14</sup>				
Effective outer cut-off radius, $R_e$ [nm]	26(4)	1150(50)				
Wilkens arrangement parameter	2.5(3)	25(1)				
Effective edge fraction, $f_E$	0.66(7)	0.99(10)				
Deformation fault probability, $\alpha$ [%]	0.7(1)	-				
Average domain size [nm]	39.5(5)	59.0(5)				
APDB model 2.I, $\delta$ ' [%]	-	2.7(17)				
APDB model 2.II, $\delta$ '' [%]	-	4.3(15)				
Cu <sub>2</sub> O phase content [wt%]	-	1.4(5)				
Unit cell parameter, $a_0$ [nm]	0.3750(2)	0.3755(1)				
R <sub>wp</sub> [%]	5.09	6.25				
R <sub>exp</sub> [%]	4.25	5.07				
GoF	1.20	1.23				



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#### nanocrystalline $CeO_2$ , TEM





#### nanocrystalline CeO<sub>2</sub>, WPPM





#### nanocrystalline CeO<sub>2</sub>, WPPM vs. TEM





Refined cell parameters increase with decreasing average grain diameter





## nanocrystalline $CeO_2$ , surface relaxation





Simulation for CeO<sub>2</sub>, lognormal distribution of spheres (average 3nm, lognormal variance 0.3), surface relaxation (A=0.05nm, affected zone B=0.3 nm), dislocations (10<sup>16</sup> m<sup>-2</sup>, R<sub>e</sub>=3nm), twins (1%) and stacking faults (2%)





# nanocrystalline CeO<sub>2</sub>, WPPM result

		WPPM	GSR-WPPM°	
				fixed
CELL PARAMETER				TIXEU !
cell parameter	(nm)	0.54153(3)	0.541134	
				P <sup>4</sup>
SIZE DISTRIBUTION (sp	herical g	rains)		
lognormal µ		1.41(2)	1.42(1)	
lognormal $\sigma$		0.355(7)	0.364(6)	
average diameter	(nm)	4.37(1)	4.40(6)	
DISLOCATIONS				
dislocation density	(m <sup>-2</sup> )	1. <b>4(10)</b> 10 <sup>16</sup>	1.08(4) 10 <sup>16</sup>	
edge dislocations content	(%)	50	50	
cutoff radius Re	(nm)	2(1)	3(1)	
A (from elastic constants)		0.1187	0.1187	
B (from elastic constants)		0.1618	0.1618	
Wilkens parameter M		0.25(1)	0.31(3)	
GRAIN SURFACE RELAXA	TION			
relaxation factor $\xi$	(nm)		0.008(3)	
decay constant $\kappa$	(nm)		0.16(4)	
STATISTICAL ESTIMATO	ORS			
Rwp		5.51	5.58	
Rexp		4.67	4.67	(°) at purpturped a const
GOF		1.18	1.20	( ) structural const



# nanocrystalline $CeO_2$ , TEM evidence







# nanocrystalline $CeO_2$ , TEM evidence







# nanocrystalline $CeO_2$ , TEM evidence







#### nanocrystalline CeO<sub>2</sub>, WPPM vs. TEM





Ceria xerogel heating and isothermal treatment: lognormal size distribution





# nanocrystalline $CeO_2$ , heating





# Ball milled nickel powder

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# Laboratory XRD result

WPPM modelling result for a Fe1.5Mo powder milled 128h





#### SR XRD result (16h milling)

Fe1.5Mo powder ball-milled for 16 hours in a Fritsch P4 planetary mill



#### SR XRD result (96h milling)

Fe1.5Mo powder ball-milled for 96 hours in a Fritsch P4 planetary mill









WPPM assuming a lognormal distribution



## Size distributions (histogram)

Reasonable agreement between a priori lognormal and 'free' histogram distribution:  $\langle D \rangle = 19.8$  (2.0) and 20.1 (3.0) nm, respectively





'Dislocation distance' versus domain size. Average number of dislocations per grain: 4 ÷ 8





Unit cell parameter: increasing with milling time. Effect of lattice defects and contamination (Cr,  $O_2$ )





#### Annealing kinetics (literature)

Problems with isothermal treatments: materials may considerably change during heating, before the isothermal treatment starts.

'Grain' size after ball milling is ~35 nm, increasing to ~70 nm during heating up to treatment temperature. Microstrain also changes (drastically drops) during heating.

Some information is lost or mingled.



FIG. 1. Isothermal evolution of  $\overline{R}$  in ball-milled, nanocrystalline Fe at the indicated annealing temperatures, as determined by a Fourier analysis of x-ray diffraction peak profiles. The straight lines are guides to the eye illustrating linear growth kinetics at initial annealing times; deviations from linearity become apparent when  $\overline{R}$  exceeds ~150 nm.


## Recovery/recrystallization

Advantage of using defect density: not affected by the recrystallization/grain coarsening transition. Ball milled Fe1.5Mo at different heating rates (2.5, 7.5, 15)



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Ball milled Fe1.5Mo at different heating rates ( $\phi$  = 2.5, 7.5, 15 °C/min): activation energy of recrystallization by Kissinger method





## Ball milled nickel powder

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### ball milled CaF<sub>2</sub>, ESEM



#### As-received powder

Acc.V Spot Magn Det WD - 5 µm 10.0 kV 5.0 4000x GSE 9.9 0.7 Torr 433587

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### ball milled CaF<sub>2</sub>, ESEM



### Powder milled 64h, $\Omega$ = 200 rpm

Large aggregates are destroyed: smaller aggregates composed of small particles are present





### ball milled CaF<sub>2</sub>, modified WH



Trend of the modified Williamson-Hall plots by increasing the milling time.

An increase in the defect content (increase in the slope of the curves) is associated to a decrease in the domain size (increase in the intercept).



### ball milled CaF<sub>2</sub>, modified WH





### ball milled CaF<sub>2</sub>, WPPM result



Modelled domain size distribution: large errors are associated to low frequencies. The average (12.9 nm) is almost the same as that obtained by assuming the distribution as being lognormal. WPPM result for fluorite powder milled 128h: two phases are present (fluorite + iron, the latter coming from the vial and balls).





## ball milled CaF<sub>2</sub>, WPPM result





### ball milled CaF<sub>2</sub>, WPPM result

A summary of the microstructural WPPM results is presented in table, together with he corresponding stored strain energy.

Milling time (h)	1	2	4	8	16	32	64	128
<d> (nm)</d>	87(27)	24(2)	28(1)	20(1)	16.9(8)	19(2)	17.3(8)	12.9(1)
$ ho_{disl} (10^{15}  m^{-2})$	2.1(3)	3.8(3)	4.6(6)	5.8(2)	7.0(20)	7.7(31)	9.6(16)	11.9(20)
R <sub>e</sub> (nm)	3(1)	4.3(1)	7.5(1)	6.4(1)	4.6(1)	7.2(1)	6.6(1)	3.4(1)
f	0.47(3)	0.65(2)	0.9(1)	0.7(1)	0.96(6)	0.87(2)	0.67(9)	0.67(2)
U <sub>strain</sub> (J/mol)	25	65	117	128	136	190	215	170

WPPM results confirm the qualitative finding of the modified Williamson Hall method, especially for very low and very high milling times where strain and size effects are dominant, respectively.

As expected, strain energy increases with increasing milling time and this can increase the reactivity of the powders.

# Conclusions



### Main advantages of the WPPM with respect to traditional methods

- correct counting statistics is used;
- problem of peak overlapping is intrinsically solved: peak profiles across the whole pattern are simultaneously refined;
- instrumental profile component can be easily included as well as appropriate background functions;
- different line profile models (e.g., dislocation, faulting, APBs, etc.) can be tested together (parameter correlations can be evaluated);
- structural constraints can be easily implemented: the WPPM algorithm can host a Rietveld routine (or vice-versa) for a simultaneous structure-microstructure refinement
- multiple phase samples can be studied (considering different microstructures) including quantitative phase analysis



For further information on: WPPM

- seeing PM2K in action
- getting a personal copy of the software

Structural/Microstructural analysis in more complex cases (<3D materials such as layered silicates, heavily faulted structures, etc.)

new DIFFaX+ release v. 2

please feel free to contact me at the conference or via e-mail (I don't bite!)







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